



# Challenges of FUSE Operations with the New Attitude Control System

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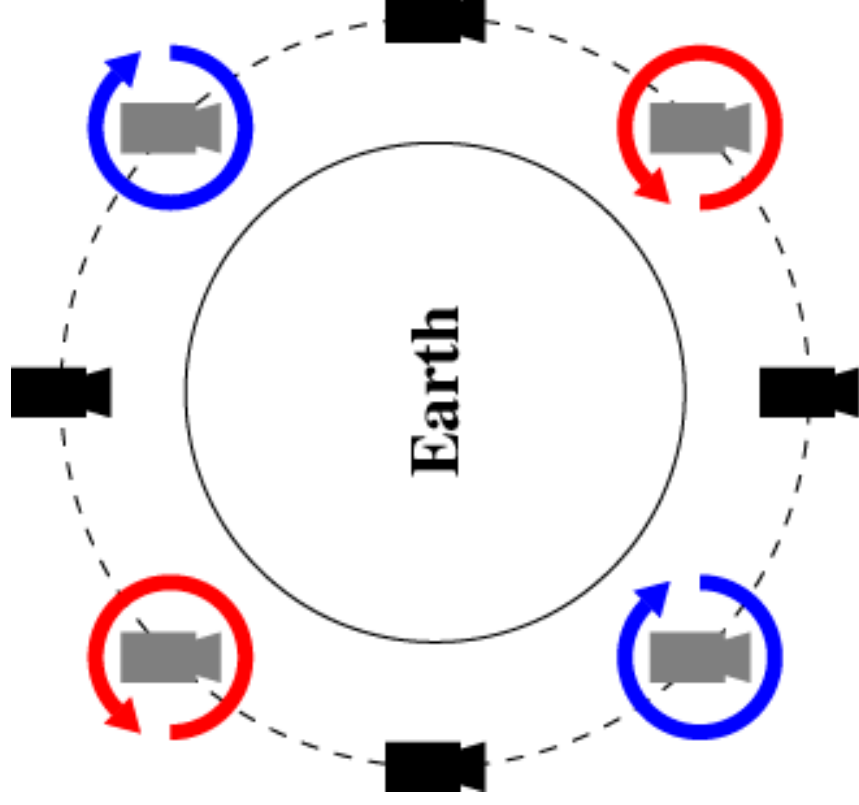
# Overview of Challenges



- ❖ Control on axes with RWAs – as good as before!
- ❖ A-axis control is now more complicated:
  - MTB torque must equal or exceed sum of disturbance torques for stable pointing
  - MTB torque must equal or exceed disturbance torques  
*AND* ramp up/ramp down torque for accurate slewing
- ❖ On-board control system simply responds to the environment, but...
- ❖ Ground-based planning software must model environment for accurate predictions

# Gravity Gradient Disturbances

- ❖ Gravity gradient is only significant external disturbance torque
- ❖ Equivalent to ‘tidal forces’
- ❖ Equation:  $\tau = \frac{3GM_{\oplus}}{r^2} R_S \times IR_S$
- ❖ Magnitude and per'-axis components depend on:
  - Spacecraft orientation
  - Instantaneous orbital parameters
- ❖ Easy to model gravity gradient torques accurately with a good orbit propagator



# Magnetic Torque Authority



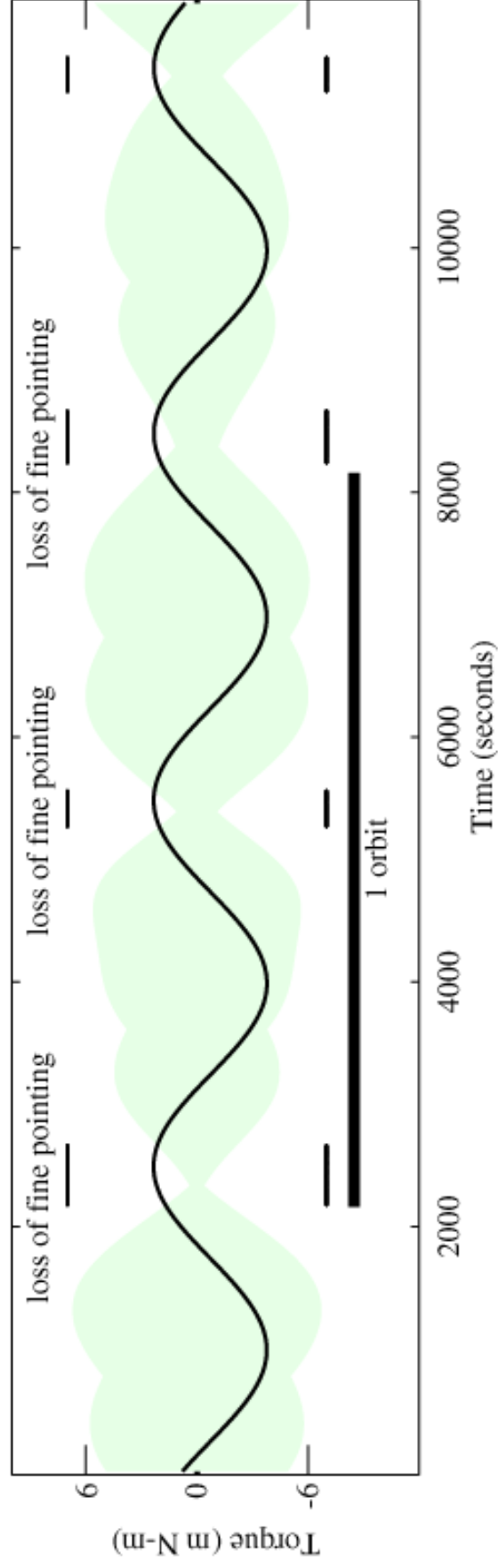
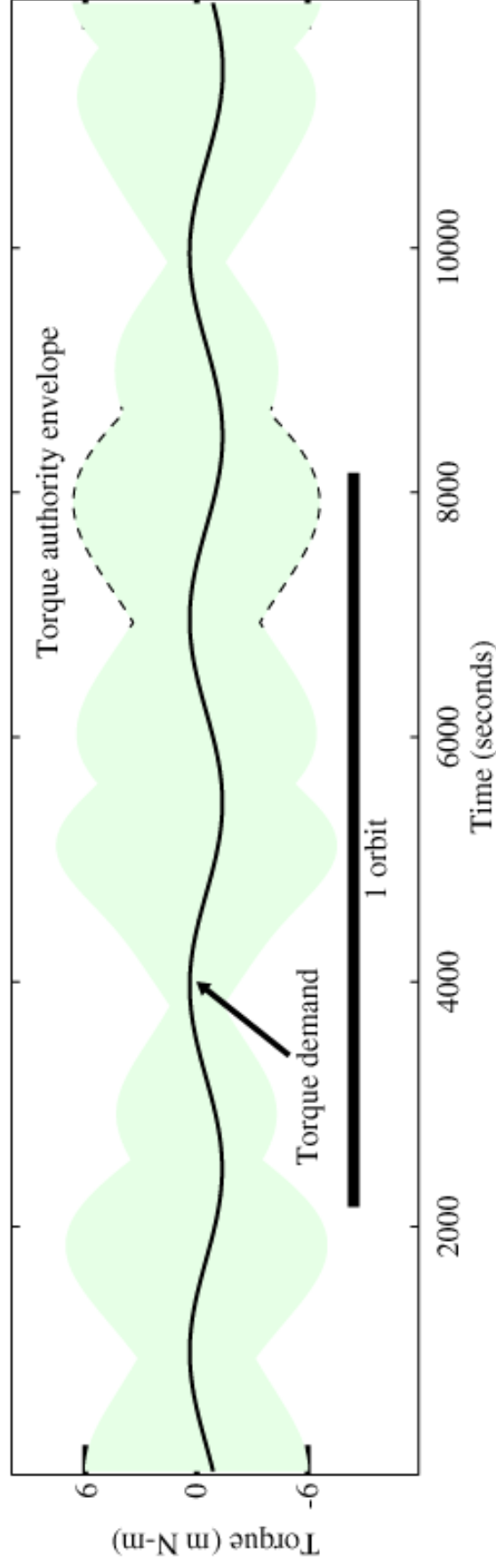
- ❖ Torques developed as control system commands
- ❖ MTBs to work against geomagnetic field
- ❖ Formula:  $\tau = \mu \times B$
- ❖ Magnetic field direction and strength varies significantly with time
- ❖ Variations are *predictable* with a good model
- ❖ MTB dipole moments were determined pre-launch exclusively for wheel unloading
  - Have to predict MTB command saturation

# Putting it all together: predicting stability



- ❖ Can generate an all-sky map by repeating calculation over many different sightlines (attitudes)
- ❖ Can generate torque authority time windows by repeating calculation over a long time span
- ❖ Regions of stability are highly variable over short timescales

# Torque Balance Examples



# A further complication: slewing

- ❖ Same principles as for predicting stable pointing, but:
  - ▶ A-axis ramp up/ramp down torque demand added to gravity gradient
  - ▶ Cross coupling of ‘gyroscopic torques’ into A-axis
  - ▶ Attitude continuously changing during slew

